A Look at Load-Distributing and Load-Sharing Anchor Systems

Presented by:

John McKently Bruce Parker Et Cedric Smith

A Look at Load-Distributing and Load-Sharing Anchor Systems

Several variations of multi-point anchors are commonly used in rescue systems when bombproof anchors (oak trees, I-beams or fire trucks) are not available. There are several schools of thought and rigging considerations regarding proper rigging technique of both "load distributing" and "load sharing" multi-point anchor systems. In order to explore how the a load is distributed both statically and during a dynamic event, we have chosen various multi-point anchor ties using a maximum anchor length of 30 centimeters (12 inches) and using a maximum 90 degree outer angle.

about the Presenters

John McKently has been with the Los Angeles County Sheriffs, Montrose Search and Rescue Team since 1974. The Team is a member of the Mountain Rescue Association (MRA) and responds to incidents ranging from car-overs and searches for overdue hikers, hunters and skiers to rescuing stranded or fallen climbers. Montrose' prime response area is approximately 500 square miles of the Angeles National Forest including Big Tujunga Canyon, most of the Angeles Crest and Angeles Forest Highways and includes two small ski areas. The team is also one of five Mine Rescue teams in California and has responded to underground emergencies throughout the state. He presently holds the rank of Reserve Commander with the Sheriff's Department and has experienced over 1700 callouts during his career with the Team. He has taught SAR Management for OES since 1988. He served on the Board of Directors of the National Association for Search and Rescue (NASAR) and was the Treasurer of that Association for four years. Active in the development of Search and Rescue standards since its inception in 1989, John served 6 years as the Chairman of ASTM Committee F-32 on Search and Rescue and authored several standards documents. After 20 years with a financial institution John is presently the School Director and Lead Instructor for CMC Rescue Inc. where he specializes in Rope Rescue, Confined Space Rescue and other specialized rescue training.

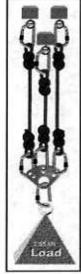
Bruce Parker is has been a Senior Lead Instructor for CMC Rescue School for 14 years. Bruce specializes in Rope Rescue, Confined Space and Rappel training. He is responsible for course development and compliance towards applicable standards such as NFPA 1670 & 1006. He is extremely concerned with rescuer and victim safety and has worked to develop and improve many products manufactured by CMC. Prior to joining the CMC Rescue team, he was the Training and Program Development Coordinator for Preparedness, Training, and Development. He researched, designed, taught, and coordinated several rescue programs for industries including: Emergency Rope Rescue and Confined Space Rescue; Response Teams: HAZWOPER; Medic First Aid Training; and EMT Training and 1 recertification. Bruce has taught Rope Rescue, Confined Space Rescue, Blood borne Pathogens, and Light Search and Rescue Training, to public agencies and private corporations. He has also designed and published safety manuals for several clients. He is active in ASTM as a member of the F32 Committee writing standards for Search and Rescue. He is rated to teach mine rescue by MSHA and is a State of California Senior Fire Instructor. Bruce has been a member of the Montrose Search and Rescue Team for 27 years, serving in all ranks including 3 years as Captain.

Cedric Smith has been an Engineering Technician at CMC Rescue since 2003. He works closely with the Product Development Committee and is responsible for product development, testing and certification. Prior to his employment with CMC he resided in Nova Scotia were he served as a volunteer firefighter with the Meteghan Fire Department as well as a member of Clare Municipal SAR. Cedric attended Seneca College in Toronto, Ontario, where he received a diploma in Fire Engineering Technology. While residing in Ontario he taught rescue courses for a recognized outdoor adventure company in the fields of Technical Rope, Swiftwater, and Ice Rescue. In addition to being an active ASTM F32 Committee member, Cedric is also a member of Santa Barbara County Search & Rescue and Santa Barbara County Air Support.

Multi-point Anchors

When rigging a rescue anchor system, finding a "bombproof" anchor point that is perfectly situated is very rare. The need to build an anchor system that corrects for bad location or spreads the load over multiple weaker points is more the norm.

There are two major types of multi-point anchors; Load Sharing and Load Distributing.



Load Sharing Anchor

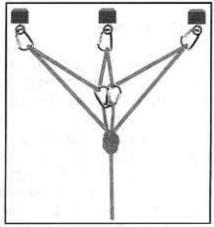
Load Sharing anchors have fixed length extensions from the various anchor points that connect together to support the load. Two factors determine how much load will end up on each anchor point. Those are the distance the anchor points are apart, which translates into the angle between the different legs, and the rigger's ability to tie the proper length extension for each point. Should one of the anchor points fail, their placement in relationship to the direction of pull will determine the resulting load on the remaining point(s). An ideal 3-point Load Sharing anchor would be similar to the one on the left. The three parallel legs would each support one third of the load. More often, the situation looks like the one on the right. The anchor points are far apart,



Load Sharing Anchor

which increases the force on each leg. If each extension isn't tied so the tension is equal to the other two, the increased force is not shared equally among the three anchor points.

Load Distributing, sometimes called Self Equalizing, anchors have variable length extensions that, in a perfect world, would allow the load to be equally distributed to all the anchor points. The angle between the anchor points also affects Load Distributing anchor systems but the "adjusting" feature of the legs tends to solve the problem of tying the legs the proper length. Previous testing has shown that due to friction within the anchor system, true equalization does not occur, hence the shift away from calling them Self Equalizing. Additionally, due to the adjustability of the extensions, if one of the anchor points fails, slack is created within the anchor system that results in dynamic loading as the load is redistributed to the remaining anchor points.



Load Distributing Anchor



Part One of these tests was designed to evaluate at how well the load is spread over 3point anchor systems and whether the variability of the Load Distributing anchor does a better job than a Load Sharing anchor at spreading out the forces.

Part Two was designed to evaluate the results of an anchor point failure. We wanted to see how much dynamic loading and load shift is created within each anchor system when different anchor points are deliberately failed.

The Test Set Up

Three anchor points were rigged on a drop tower with Load Cells to measure the force on each. Anchor Point #1 was on the left with an Omega 3000# load cell. Anchor Point #2 was in the middle with an Omega 5000# load cell and Anchor Point #3 was on the right with an Omega 5000# load cell. An Omega 10,000# load cell was between the anchor and the load to measure the maximum arrest force. A pneumatically controlled release was used to simulate a failure of the anchor points. The load was 2.65 kN (595 lbf).

Do to limited testing time, one variable that would reduce the maximum arrest force slightly was eliminated. Knots tighten when dynamically loaded which helps to resolve some of the dynamic energy thereby reducing the maximum arrest force. For consistency the test mass was dropped on each rope anchor system three times and each webbing anchor system once, to set the knots.

Test Procedure

After each anchor system was rigged and visually equalized, the mass was lowered on to it. The "A" Test results indicate the force on each anchor point at that time. Then one of the anchor point was released, simulating a

each anchor point at that time. Then one of
the anchor point was released, simulating a
sudden failure, and the maximum force on the remaining anchor points and the load
was recorded in the "B" Test. The extension of the anchor system was also recorded.
Another parameter that should be considered is the sideways shift when an anchor
point fails. Excessive sideways movement could cause the rope to move off edge
protection resulting in rope damage or failure. When the #2 Anchor Point (the center
one) was failed there was no shift as the forces transferred to the outside anchor points.

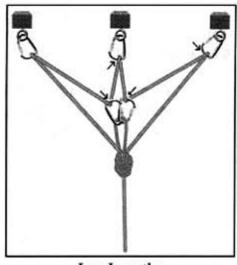




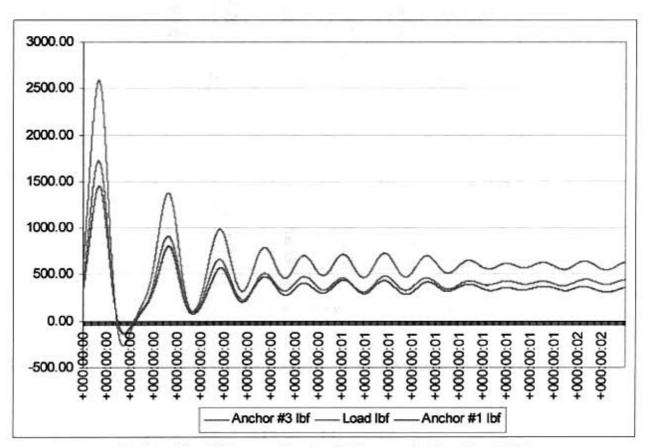
When one of the outside anchor points was failed, the load shifted to center between the two remaining anchor points, in this case about 43 cm (17").

The leg lengths on the Load Distributing anchors were measured from where the rope bends around the carabiners.

Forces for the two remaining anchor points and the load was charted for each test. The pattern for each test was similar so only one example has been included.



Leg Lengths



Anchor #3 = 1721

Load = 2592

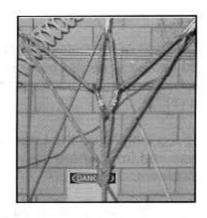
Anchor #1 = 1454

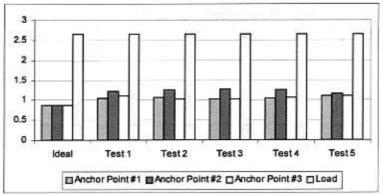
Anchor #1 - A Double Loop Figure Eight knot was tied with 12.5 mm Static Pro kernmantle rope and rigged into a Load Distributing anchor.

Legs - 29cm (11.5"), 16cm (6.5"), 29cm (11.5")

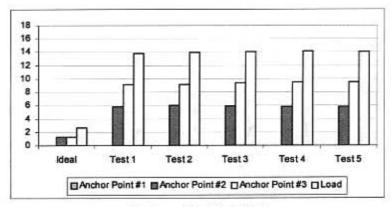
B-1 Extension - 27.1cm (10.7")

B-2 Extension - 12.8cm (5")

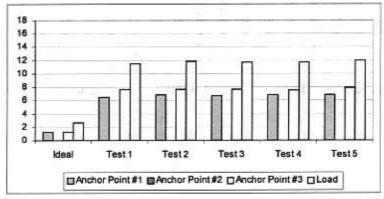




Anchor #1 - Test A



Anchor #1 - Test B-1



Anchor #1 - Test B-2

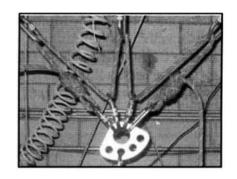


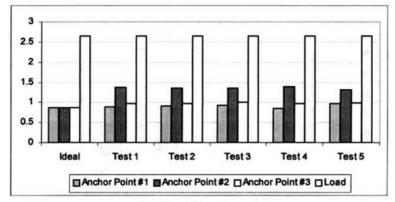
Anchor #2 - A Load Distributing anchor tied with 12.5mm Static Kernmantle rope using an anchor plate as a collection point.

Legs - 31cm (12.25"), 20cm (8"), 31cm (12.25")

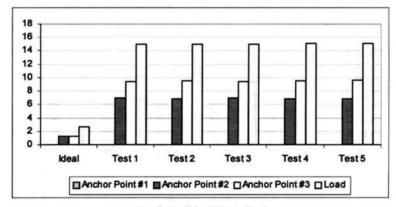
B-1 Extension - 25.6cm (10")

B-2 Extension - 16.3cm (6.4")

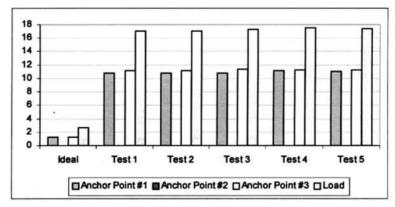




Anchor #2 - Test A



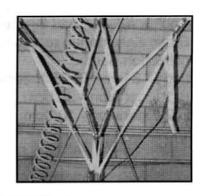
Anchor #2 - Test B-1

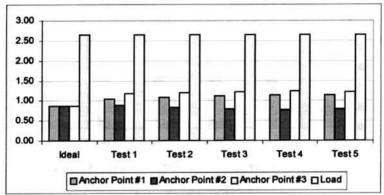


Anchor #2 - Test B-2

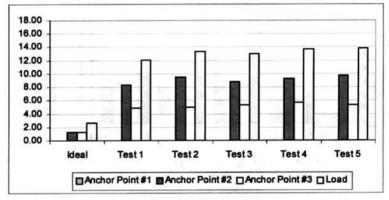


Anchor #3 - A 3-way Multi-point Load Distributing anchor made with 1" Nylon tubular webbing.
Legs - 30cm (12"), 30cm (12"), 30cm (12")
B-1 Extension - 23.1cm (9.1")
B-2 Extension - 1.5cm (0.6")

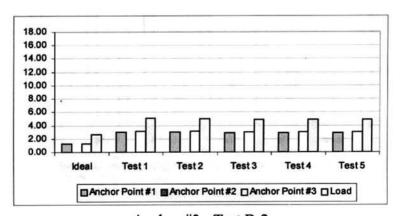




Anchor #3 - Test A



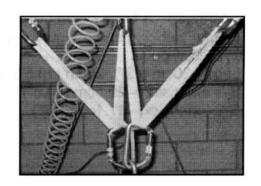
Anchor #3 - Test B-1

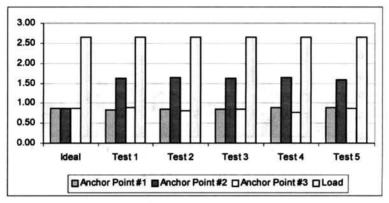


Anchor #3 - Test B-2

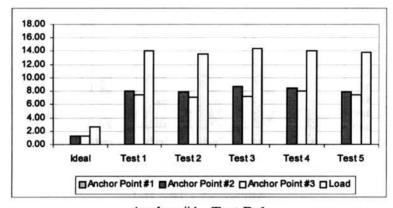


Anchor #4 - A Sliding X Load Distributing anchor made with 1" Nylon tubular webbing.
Legs - 30cm (12"), 21cm (8.5"), 30cm (12")
B-1 Extension - 27.6cm (10.9")
B-2 Extension - 15.5cm (6")

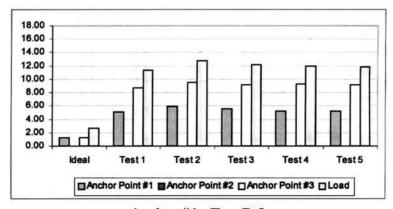




Anchor #4 - Test A



Anchor #4 - Test B-1



Anchor #4 - Test B-2

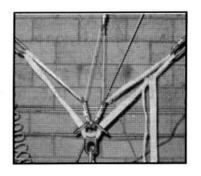


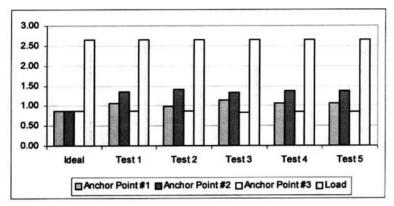
Anchor #5 - A Load Distributing anchor made with 1" Nylon tubular webbing and a Figure Eight descender as a sliding collection point.

Legs - 30cm (12"), 26cm (10.5"), 30cm (12")

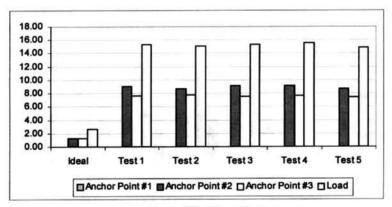
B-1 Extension - 29.5cm (11.6")

B-2 Extension - 17.1cm (6.7")

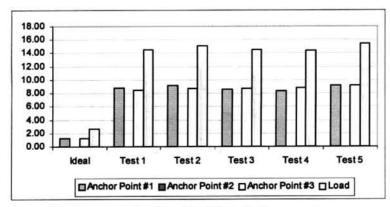




Anchor #5 - Test A



Anchor #5 - Test B-1



Anchor #5 - Test B-2

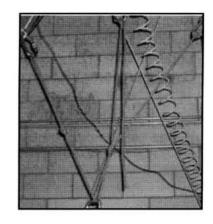


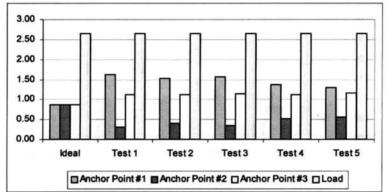
Anchor #6 - Equalette - A Load Distributing anchor made with 8 mm Nylon cord. This was found in the book <u>Climbing Anchors</u>. As rigged it is a two-point LDA with one leg attached to a single anchor point and the second leg attached to a two-pint load sharing anchor.

Legs - 30cm (12"), 20cm (8")

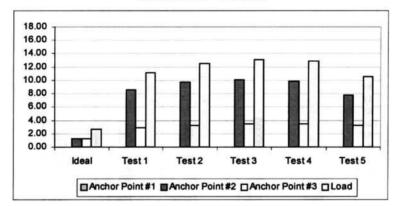
B-1 Extension - 59.4cm (23.4")

B-2 Extension - 2.4cm (1")

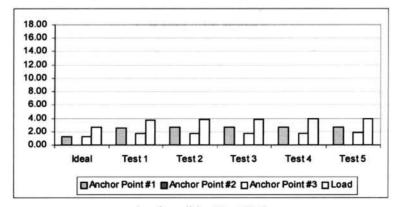




Anchor #6 - Test A



Anchor #6 - Test B-1



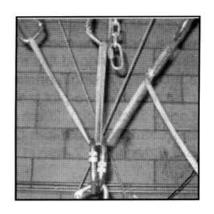
Anchor #6 - Test B-2

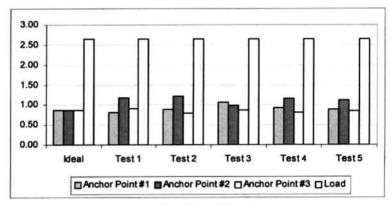


Anchor #7 - A Load Distributing anchor made with ½" Nylon/Spectra webbing.

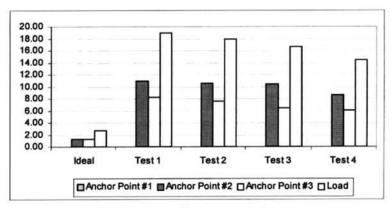
Legs - 30cm (12"), 25cm (10"), 30cm (12")

B-1 Extension - 22.5cm (8.8")





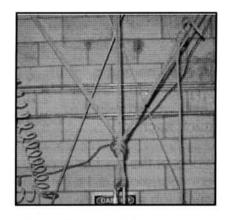
Anchor #7 - Test A

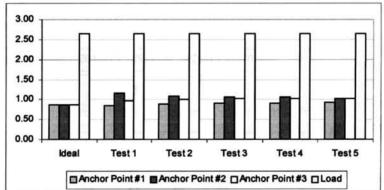


Anchor #7 - Test B-1

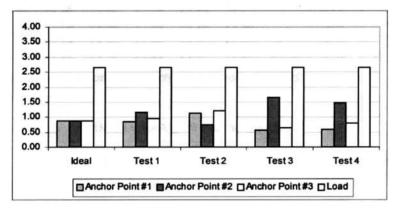
Anchor #8 - A Load Sharing anchor made with 8 mm cord.

B-1 Extension - 2.5cm (1")

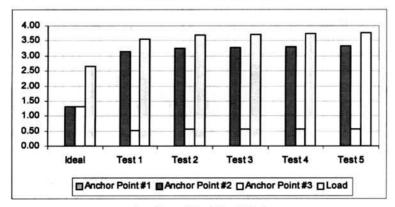




Anchor #8 - Test A



Anchor #8 - Test A-2



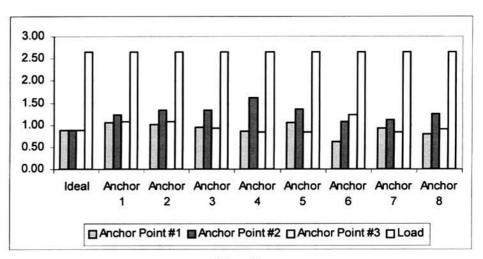
Anchor #8 - Test B-1



Conclusions

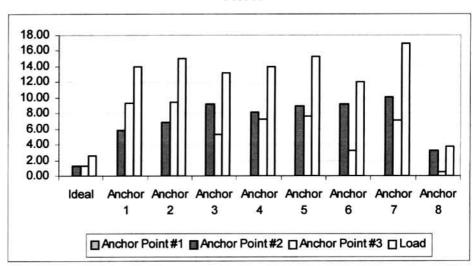
These charts are averages of the five tests we did with each anchor.

None of the anchor configurations did a great job at equally sharing the load.



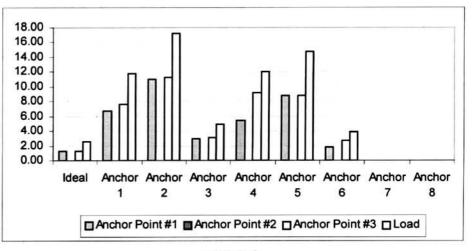
Test A

When anchor point #1 failed all the Load Distributing Anchors developed high Maximum Arrest Forces with poor equalization. The Load Sharing anchor had a much lower MAF but 87% of the load ended up on one anchor point.



Test B-1

When anchor point #2 failed, some of the Load Distributing anchors performed better than others with relatively small MAF and good equalization.



Test B-2



	ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#1 - LDA - Double Loop	Figure Eight		1A	1.05	1.22	1.11	2.65	
CMC Static Pro - 12.5 r	nm		1B	0.00	5.75	9.23	13.77	26.34
Legs - 29cm (11.5")	16cm (6.5")	29cm (11.5")	2A	1.07	1.26	1.03	2.65	
#1	#2	#3	2B	0.00	6.01	9.21	13.98	27.61
-602	P		3A	1.03	1.28	1.03	2.65	
といって	M		3B	0.00	5.87	9.46	14.09	27.31
E 135	_///		4A	1.05	1.25	1.06	2.65	
134		- //	4B	0.00	5.84	9.49	14.11	27.31
1 1 1			5A	1.11	1.17	1.10	2.65	
	14		5B	0.00	5.77	9.47	14.06	27.31
			Mean A	1.06	1.24	1.07	2.65	
- X		1	Mean B-1	0.00	5.84	9.37	14.00	27.18
			6A	0.90	1.13	1.09	2.65	
1 /			6B	6.47	0.00	7.65	11.53	13.00
	11/		7A	1.01	1.07	1.10	2.65	
1			7B	6.85	0.00	7.65	11.84	12.70
	(DANC)		8A	0.94	1.13	1.07	2.65	
	MI		8B	6.74	0.00	7.67	11.77	12.70
	4 /		9A	0.92	1.19	1.01	2.65	
	#4		9B	6.85	0.00	7.58	11.77	13.00
			10A	1.09	0.85	1.27	2.65	
			10B	6.80	0.00	7.86	11.98	12.70
			Mean A	0.97	1.07	1.11	2.65	
			Mean B-2	6.74	0.00	7.68	11.78	12.83

	ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#2 - LDA - Anchor Plate	•		11A	0.98	1.37	1.05	2.65	
CMC Static Pro - 12.5 r	nm		11B	0.00	7.02	9.38	15.01	24.13
Legs - 31cm (12.25")	20cm (8")	31cm (12.25")	12A	1.02	1.32	1.07	2.65	
			12B	0.00	6.81	9.52	14.95	27.31
#1	#2	#3	13A	0.98	1.38	1.03	2.65	
		1	13B	0.00	6.93	9.41	14.98	24.57
	- 11/		14A	1.02	1.32	1.09	2.65	
13/	- II		14B	0.00	6.87	9.57	15.07	24.13
	- 11		15A	1.05	1.28	1.12	2.65	
	- /1	FI	15B	0.00	6.81	9.66	15.07	27.94
			Mean A	1.01	1.33	1.07	2.65	
	1 / /r		Mean B-1	0.00	6.89	9.51	15.02	25.63
			16A	0.89	1.37	0.97	2.65	
127			16B	10.79	0.00	11.16	17.06	16.51
22	1		17A	0.91	1.36	0.96	2.65	
100			17B	10.85	0.00	11.12	17.10	15.88
	CONTRACTOR OF THE PERSON OF TH		18A	0.92	1.36	1.00	2.65	
	#4		18B	10.84	0.00	11.40	17.31	16.51
			19A	0.86	1.40	0.96	2.65	
			19B	11.16	0.00	11.26	17.48	16.51
			20A	0.96	1.31	0.98	2.65	
			20B	11.08	0.00	11.29	17.45	16.51
			Mean A	0.91	1.36	0.97	2.65	
			Mean B-2	10.95	0.00	11.25	17.28	16.38

	ANCHOR		Test#	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#3 - LDA - 3-Way Mu	Ilti-point Anchor		21A	1.01	1.26	0.97	2.65	
1" Tubular Nylon We	bbing		21B	0.00	8.37	4.92	12.07	22.86
Legs - 30cm (12")	30cm (12")	30cm (12")	22A	0.89	1.44	0.84	2.65	
			22B	0.00	9.53	5.00	13.34	22.86
#1	#2	#3	23A	0.98	1.27	0.99	2.65	
	THE STATE OF THE S		23B	0.00	8.88	5.38	12.95	22.86
	11/2	.91	24A	0.95	1.29	0.98	2.65	
	S/1		24B	0.00	9.29	5.64	13.66	23.50
	ISM ///	11	25A	0.88	1.41	0.88	2.65	
The second second	341	LLV	25B	0.00	9.72	5.37	13.86	23.81
	31/1/2		Mean A	0.94	1.33	0.93	2.65	
		_ () A	Mean B-1	0.00	9.16	5.26	13.18	23.19
16	N III		26A	1.05	0.89	1.18	2.65	
			26B	2.99	0.00	3.15	5.08	1.91
3	1 47 1		27A	1.09	0.84	1.20	2.65	
			27B	2.97	0.00	3.09	5.00	1.57
8/	17		28A	1.13	0.80	1.22	2.65	
(2)			28B	2.93	0.00	3.03	4.91	2.54
	#4		29A	1.15	0.77	1.23	2.65	
			29B	2.90	0.00	2.97	4.82	0.64
			30A	1.14	0.79	1.21	2.65	
			30B	2.94	0.00	3.05	4.92	1.27
			Mean A	1.11	0.81	1.21	2.65	
			Mean B-2	2.95	0.00	3.06	4.94	1.57

	ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#4 - LDA - Sliding X	Anchor		31A	0.83	1.62	0.89	2.65	
1" Nylon Tubular We	bbing		31B	0.00	8.07	7.44	14.07	27.94
Legs - 30cm (12")	21cm (8.5")	30cm (12")	32A	0.86	1.65	0.81	2.65	
Stal 966 254			32B	0.00	7.90	7.10	13.54	27.94
#1	#2	#3	33A	0.86	1.62	0.85	2.65	
* X	2/4	15	33B	0.00	8.67	7.17	14.38	27.31
	32/1/		34A	0.89	1.65	0.78	2.65	
	ST/ 11		34B	0.00	8.50	6.99	14.09	27.31
	3/ 11		35A	0.89	1.59	0.88	2.65	
	有一局		35B	0.00	7.88	7.42	13.86	27.94
	AIL		Mean A	0.87	1.62	0.84	2.65	
			Mean B-1	0.00	8.21	7.22	13.99	27.69
	18/18		36A	0.73	1.42	0.95	2.65	
		N A	36B	5.12	0.00	8.75	11.40	15.54
			37A	0.80	1.40	0.92	2.65	
	#4		37B	5.95	0.00	9.50	12.73	15.88
			38A	0.81	1.40	0.91	2.65	
			38B	5.60	0.00	9.22	12.20	15.24
			39A	0.76	1.40	0.95	2.65	
			39B	5.28	0.00	9.24	11.98	15.24
			40A	0.78	1.35	1.00	2.65	
			40B	5.20	0.00	9.12	11.82	15.88
			Mean A	0.77	1.39	0.94	2.65	
			Mean B-2	5.43	0.00	9.17	12.02	15.54

	Service Contracts of Services Contracts of S		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#5 - LDA - Figure Ei	ght Descender		41A	1.06	1.36	0.88	2.65	
1" N ylon Tubular We	ebbing		41B	0.00	9.02	7.66	15.35	29.21
Legs - 30cm (12")	26cm (10.5")	30cm (12")	42A	0.98	1.42	0.87	2.65	
			42B	0.00	8.73	7.74	15.08	29.21
#1	#2	#3	43A	1.14	1.33	0.83	2.65	
1 1			43B	0.00	9.12	7.54	15.33	29.85
	11	1	44A	1.06	1.38	0.85	2.65	
		1	44B	0.00	9.20	7.68	15.54	29.21
*			45A	1.06	1.37	0.85	2.65	
			45B	0.00	8.72	7.48	14.89	30.48
			Mean A	1.06	1.37	0.85	2.65	
			Mean B-1	0.00	8.96	7.62	15.24	29.59
			46A	0.87	1.25	0.97	2.65	
3	FF		46B	8.85	0.00	8.52	14.54	17.78
31	1		47A	0.88	1.24	0.97	2.65	
			47B	9.22	0.00	8.76	15.10	18.42
2	R		48A	0.90	1.26	0.92	2.65	
		WI bear	48B	8.55	0.00	8.71	14.47	15.88
	#4		49A	0.88	1.23	0.97	2.65	
			49B	8.31	0.00	8.88	14.43	15.88
			50A	0.89	1.22	0.99	2.65	
			50B	9.19	0.00	9.13	15.40	17.78
			Mean A	0.89	1.24	0.97	2.65	
			Mean B-2	8.83	0.00	8.80	14.79	17.15

	ANCHOR		Test#	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#6 - LDA - Equalette (C	limbing Anchors)		51A	1.62	0.31	1.12	2.65	
8 mm Nylon Cord			51B	0.00	8.64	2.93	11.17	57.15
Legs - 30cm (12")	20cm (8")		52A	1.53	0.40	1.12	2.65	
			52B	0.00	9.75	3.24	12.56	57.79
#1	#2	#3	53A	1.56	0.34	1.14	2.65	
	18	2/. 1	53B	0.00	10.11	3.49	13.17	59.69
2 1			54A	1.37	0.53	1.12	2.65	
16		72	54B	0.00	9.88	3.44	12.89	61.60
N		12 /	55A	1.29	0.57	1.17	2.65	
		12,	55B	0.00	7.80	3.20	10.52	60.96
TO Valle		10	Mean A	1.48	0.43	1.11	2.65	
			Mean B-1	0.00	9.24	3.26	12.06	59.44
			56A	1.24	1.04	0.66	2.65	
		1=	56B	2.56	0.00	1.69	3.70	3.18
			57A	1.23	1.07	0.63	2.65	
			57B	2.64	0.00	1.74	3.81	2.54
The state of the s	1-11-	10	58A	1.22	1.08	0.63	2.65	
		1	58B	2.67	0.00	1.76	3.86	1.91
data and the second	-	The state of the s	59A	1.23	1.07	0.62	2.65	
	#4	•	59B	2.71	0.00	1.78	3.91	2.54
			60A	1.19	1.11	0.61	2.65	
			60B	2.70	0.00	1.81	3.93	2.54
			Mean A	1.22	1.07	0.63	2.65	
			Mean B-2	2.66	0.00	1.76	3.84	2.54

CMC Rescue **Multi-point Anchor Tests** 2007 Force in kN

ANCHOR	Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#7 - LDA - 3-point Webbing Anchor	61A	0.81	1.18	0.91	2.65	
.5" Nylon/Spectra Webbing	61B	0.00	10.99	8.28	18.98	22.23
Legs - 30cm (12") 25cm (10")	30cm (12") 62A	0.89	1.21	0.80	2.65	
>\	62B	0.00	10.56	7.64	17.92	22.86
	63A	1.07	0.98	0.88	2.65	
1 19/1	63B	0.00	10.39	6.50	16.66	21.59
	64A	0.93	1.17	0.81	2.65	
	64B	0.00	8.66	6.04	14.50	23.50
	65A	0.90	1.13	0.86	2.65	
7.1	65B		. = 1100. Fu			Fail
	Mean A	0.92	1.13	0.85	2.65	
	Mean B-1	0.00	10.15	7.12	17.01	22.56

	ANCHOR	L	Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension cm
#8 - LSA - Cordelet	tte		66A	0.85	1.17	0.96	2.65	
8 mm Nylon Cord			66B	0.00	3.14	0.52	3.56	1.91
#1	#2	#3	67A	0.90	1.08	1.01	2.65	
	\ Y	9011	67B	0.00	3.24	0.56	3.68	2.54
		- (//X)	68A	0.91	1.06	1.02	2.65	
		1 11/	68B	0.00	3.28	0.56	3.72	3.18
	1/1/		69A	0.91	1.06	1.02	2.65	
			69B	0.00	3.30	0.56	3.75	2.54
51	× 1	//	70A	0.93	1.03	1.03	2.65	
3	T-/-	# T	70B	0.00	3.32	0.58	3.78	2.54
2	1/1/1		Mean A	0.90	1.08	1.01	2.65	
Dippoo	1/1	1 / 1	Mean B-1	0.00	3.26	0.56	3.70	2.54
2	1		71A	1.14	0.75	1.21	2.65	
18	1 4		71B					
117	(DAI II)		72A	0.56	1.65	0.65	2.65	
	#4		72B					
			73A	0.60	1.48	0.81	2.65	
			73B					
			74A	0.85	1.17	0.96	2.65	
			74B					
			75A					
			75B					
			Mean A	0.79	1.26	0.91	2.65	
							-1	

	ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
#1 - LDA - Double Loo	p Figure Eight		1A	235	275	250	595	10:=
CMC Static Pro - 12.5	mm		1B	0	1292	2075	3096	10.37
Legs - 29cm (11.5")	16cm (6.5")	29cm (11.5")	2A	240	283	231	595	
#1	#2	#3	2B	0	1350	2070	3143	10.87
Cir.	7	No state	3A	232	288	232	595	
といって			3B	0	1319	2126	3168	10.75
6135	_//		4A	236	280	239	595	
130			4B	0	1314	2134	3173	10.75
111	VIII		5A	250	264	247	595	
	N		5B	0	1297	2130	3160	10.75
	1 3/3		Mean A	239	278	240	595	
1		1	Mean B-1	0	1314	2107	3148	10.70
			6A	202	253	245	595	
1	P 11		6B	1454	0	1720	2592	5.12
1111	111	1	7A	227	240	248	595	
+1			7B	1539	0	1720	2661	5.00
	(DANC)	1	8A	211	253	240	595	
1/	XT		8B	1515	0	1725	2645	5.00
WI I			9A	206	267	227	595	
	#4		9B	1539	0	1703	2646	5.12
			10A	244	192	285	595	
			10B	1529	0	1768	2694	5.00
			Mean A	218	241	249	595	
			Mean B-2	1515	0	1727	2648	5.05

	ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
#2 - LDA - Anchor Plate	е		11A	220	307	237	595	
CMC Static Pro - 12.5 i	mm		11B	0	1579	2109	3374	9.50
Legs - 31cm (12.25")	20cm (8")	31cm (12.25")	12A	230	297	241	595	
1			12B	0	1531	2140	3360	10.75
#1	#2	#3	13A	221	310	232	595	
	-	-	13B	0	1559	2116	3368	9.68
	M/		14A	229	297	245	595	
	> IV		14B	0	1545	2151	3388	9.50
2 Till mention	- 1/1		15A	235	287	251	595	
	2 //	FI	15B	0	1532	2172	3389	11.00
			Mean A	227	300	241	595	
	A MARIE		Mean B-1	0	1549	2138	3376	10.09
			16A	199	307	219	595	
127	1		16B	2425	0	2509	3836	6.50
202	-		17A	205	306	215	595	
113			17B	2440	0	2501	3844	6.25
			18A	206	306	224	595	
	#4		18B	2438	0	2563	3891	6.50
			19A	193	315	215	595	
			19B	2510	0	2532	3930	6.50
			20A	215	294	220	595	
			20B	2490	0	2539	3922	6.50
			Mean A	204	306	219	595	
			Mean B-2	2461	0	2529	3885	6.45

	ANCHOR		Test#	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
#3 - LDA - 3-Way M	ulti-point Anchor		21A	228	284	219	595	
1" Tubular Nylon We	ebbing		21B	0	1881	1105	2714	9.00
Legs - 30cm (12")	30cm (12")	30cm (12")	22A	201	324	188	595	
			22B	0	2142	1123	3000	9.00
#1	#2	#3	23A	221	285	222	595	
1	1		23B	0	1997	1209	2912	9.00
	VIE		24A	213	291	220	595	
-11	SIL		24B	0	2089	1268	3070	9.25
	-11	11	25A	198	316	198	595	
-	311		25B	0	2185	1208	3116	9.38
			Mean A	212	300	209	595	
		_ / 4/	Mean B-1	0	2059	1183	2962	9.13
1 6	N III		26A	237	199	266	595	
			26B	673	0	708	1141	0.75
0			27A	246	188	270	595	
			27B	668	0	694	1123	0.62
5/	VIT	a essements	28A	253	179	274	595	
100	TINE	A STATE OF THE STA	28B	659	0	681	1104	1.00
	#4		29A	258	173	277	595	
			29B	652	0	668	1083	0.25
			30A	257	178	273	595	
			30B	662	0	685	1106	0.50
			Mean A	250	183	272	595	
			Mean B-2	663	0	687	1111	0.62

	ANCHOR		Test#	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
#4 - LDA - Sliding X	Anchor		31A	187	364	200	595	
1" Nylon Tubular We	ebbing		31B	0	1815	1672	3163	11.00
Legs - 30cm (12")	21cm (8.5")	30cm (12")	32A	194	370	182	595	
			32B	0	1775	1597	3044	11.00
#1	#2	#3	33A	193	365	190	595	
* *	- A	15	33B	0	1950	1613	3233	10.75
	39/11_		34A	200	370	175	595	
	37/11		34B	0	1912	1571	3168	10.75
	37/		35A	199	357	197	595	
	4		35B	0	1771	1668	3116	11.00
	MIL		Mean A	195	365	189	595	
		REPORT FORM	Mean B-1	0	1845	1624	3145	10.90
			36A	165	319	213	595	
		N	36B	1150	0	1968	2562	6.12
8	1		37A	179	314	207	595	
	#4		37B	1337	0	2135	2861	6.25
			38A	181	315	204	595	
			38B	1258	0	2073	2743	6.00
			39A	171	315	214	595	
			39B	1187	0	2077	2694	6.00
			40A	175	303	224	595	
			40B	1168	0	2051	2657	6.25
			Mean A	174	313	212	595	
			Mean B-2	1220	0	2061	2703	6.12

#5 - LDA - Figure Eight Descender 1" Nylon Tubular Webbing Legs - 30cm (12") 26cm (10.5") 30cm (12")			Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
			41A	239	306	197	595	
			41B	0	2027	1722	3451	11.50
			42A	220	320	195	595	
			42B	0	1962	1740	3391	11.50
#1	#2	#3	43A	257	298	187	595	
			43B	0	2050	1695	3446	11.75
	1 1	1	44A	238	310	190	595	
		1	44B	0	2069	1726	3493	11.50
	Y.		45A	238	309	192	595	
			45B	0	1960	1682	3348	12.00
			Mean A	238	309	192	595	
			Mean B-1	0	2014	1713	3426	11.65
,			46A	195	281	219	595	
沙里 医细胞腺	A TEF	STREET OF	46B	1989	0	1915	3269	7.00
3			47A	198	278	218	595	
			47B	2073	0	1970	3394	7.25
2	/P		48A	203	283	206	595	
		The second	48B	1922	0	1957	3254	6.25
	#4		49A	198	277	218	595	
			49B	1869	0	1996	3244	6.25
			50A	199	274	222	595	
			50B	2067	0	2052	3461	7.00
			Mean A	199	279	217	595	
			Mean B-2	1984	0	1978	3324	6.75

#6 - LDA - Equalette (Climbing Anchors) 8 mm Nylon Cord Legs - 30cm (12") 20cm (8")			Test#	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
			51A	365	70	252	595	
			51B	0	1943	659	2512	22.50
			52A	344	89	252	595	
			52B	0	2193	728	2824	22.75
#1	#2	#3	53A	351	77	257	595	
11/		2/ 1	53B	0	2273	784	2960	23.50
5			54A	309	120	252	595	
			54B	0	2222	773	2897	24.25
			55A	289	129	263	595	
			55B	0	1753	719	2364	24.00
			Mean A	332	97	250	595	
			Mean B-1	0	2077	733	2711	23.40
			56A	279	233	148	595	
原层层型		13	56B	576	0	380	831	1.25
	1 14		57A	276	240	142	595	
		1	57B	593	0	392	857	1.00
- Lude	1	10	58A	275	242	141	595	
The same	1/// 1	TE	58B	601	0	396	867	0.75
NAME OF TAXABLE PARTY.		1	59A	277	241	140	595	
#4		59B	609	0	400	878	1.00	
			60A	267	250	138	595	
			60B	607	0	406	883	1.00
			Mean A	275	241	142	595	
			Mean B-2	597	0	395	863	1.00

ANCHOR		Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension "
#7 - LDA - 3-point Wel	61A	183 0	265 2470	205 1862	595 4266	8.75	
.5" Nylon/Spectra Webbing							61B
Legs - 30cm (12")	25cm (10") 30cm (12")	62A	199	273	179	595	
	A & h / /	62B	0	2374	1717	4028	9.00
		63A	240	221	198	595	
		63B	0	2336	1462	3745	8.50
		64A	208	262	181	595	
		64B	0	1947	1358	3260	9.25
	65A	203	255	193	595		
7.1		65B					Fail
100000		Mean A	207	255	191	595	
		Mean B-1	0	2282	1600	3825	8.88

#8 - LSA - Cordelette 8 mm Nylon Cord			Test #	MF on #1	MF on #2	MF on #3	MF on #4	Extension '
			66A	190 0	263 707	216 118	595 800	0.75
			66B					
#1	#2	#3	67A	203	243	228	595	
	N/	93/1	67B	0	728	127	828	1.00
			68A	205	239	229	595	
1		100	68B	0	738	126	836	1.25
	1	//	69A	205	239	229	595	
			69B	0	741	127	842	1.00
3 1		1/	70A	209	232	232	595	
		1	70B	0	747	130	850	1.00
9	1		Mean A	202	243	227	595	
Managar.	1	1 / 11	Mean B-1	0	732	126	831	1.00
3	1		71A	257	168	271	595	
15			71B					
DUTY COAL D			72A	126	372	146	595	
#4		72B					=	
			73A	134	332	183	595	
			73B					
			74A	190	263	216	595	
			74B					
			75A					
			75B					
			Mean A	176	283	204	595	